

1 Q. Please provide a copy of the analysis that was carried out in June and July of 2010
2 which confirmed that the 900 MW HVDC link would require a minimum operating
3 voltage of 320 kV as referenced in Exhibit 30, Section 4, paragraph 4.
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6 A. For analysis the maximum HVdc system losses has been set at 10% (worst case) in
7 order to prepare a load flow model of the scheme. It must be noted that a detailed
8 conductor and voltage optimization will be required in final design. For analysis
9 purposes it is assumed that the converter stations will account for 2% of the system
10 losses. At this point in time the “largest” standard conductor in the Canadian Alcan
11 catalog is selected. The conductor is a 55.88 mm, 91 strand, 3640 kcmil, A1 (ASC)
12 conductor with R_{dc} at 20 C = 0.01568 Ω /km and a rated tensile strength of 304 kN.
13

14 There is a total of 1038 km of overhead line between Muskrat Falls and Soldiers
15 Pond. The submarine cable across the Strait of Belle Isle is assume to be an 1800
16 mm² copper cable with R_{dc} at 20 C = 0.0098 Ω /km. The cable route is estimated to
17 be 30 km in length.
18

19 The total resistance per pole equals:

20 $R_{dc} \text{ at } 20 \text{ C} = (1038 * 0.01568) + (30 * 0.0098) = 16.5698 \text{ } \Omega/\text{pole}$
21

22 At 450 MW per pole the pole losses, excluding the converter station losses, should
23 be less than or equal to 36 MW. The pole current is calculated as:

24 $P_{loss} = I^2 R_{dc} \text{ at } 20^\circ\text{C}$

25 $36 \text{ MW} = I^2 (16.5698 \text{ } \Omega/\text{pole})$

26 $I = 1473.9 \text{ Adc/pole}$
27

1 To send 450 MW/pole assuming a 1474 A pole current, the sending end voltage is
2 calculated as:

3
4
$$P = I * V$$

5
$$450 \text{ MW} = 1474 \text{ A}_{dc} * V$$

6
$$V = 305.2 \text{ kV}$$

7

8 The resultant nominal 900 MW HVdc system ratings are:

- 9
10 • $\pm 320 \text{ kV}$;
11 • pole current of 1406 A; and
12 • losses of 41.8 MW/pole or 83.6 MW/bipole – 816.4 MW receiving end.